

## Technology for Manufacturing Working Substances for Thermoelements Branches and Determination of their Thermoelectric Characteristics

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### ABSTRACT

*The article discusses the technology of producing thermoelectric materials under inert gas pressure, which makes it possible to provide reproducible results from melting to melting and to synthesize sufficiently large amounts of a working substance.*

**KEYWORDS:** *Thermoelectric materials, solid solutions, thermo-EMF, semiconductor materials Bi<sub>2</sub>Te<sub>3</sub>, Bi<sub>2</sub>Se<sub>3</sub>, charge, tellurium, selenium, lead, crucible.*

**Introduction.** The quality of thermoelectric alloys depends not only on the composition of solid solutions, but also on the purity of the initial components. In practice, it is convenient to characterize the feedstock by the thermoelectric properties of the base (unalloyed material) alloyed from this feedstock. Quality control can also be carried out on the basis of rigorous analysis of the original alloy components. However, in the case of multicomponent connections, this method is not always the fastest, cheapest and most importantly, reliable. Therefore, the search for technological ways of optimizing thermoelectric material should be carried out in a single cycle of obtaining the base and its alloying.

### Obtaining a working substance based on Bi<sub>2</sub>Te<sub>3</sub> - Bi<sub>2</sub>Se<sub>3</sub>

For the preparation of alloys of the required composition, the initial components of the following purity were used: bismuth GOST 10928-64, grade VCh-00, tellurium GOST 9514-60, grade TA-1, selenium for rectifiers GOST 6738-53. The composition of the solid solution corresponding to 80 mol% was chosen as the n-type base. Bi<sub>2</sub>Te<sub>3</sub> and 20 mol% Bi<sub>2</sub>Se<sub>3</sub>.

The charge was loaded in the following order: Selenium was loaded on the bottom of the crucible, then tellurium, and bismuth on top. Tellurium and selenium were used as super stoichiometric chalcogens introduced into the charge. [2]

The experiment was carried out with Bi<sub>2</sub>Te<sub>3</sub> - Bi<sub>2</sub>Se<sub>3</sub> mixtures in amounts of 20, 60, and 100 g by fusing the initial components in a quartz crucible with a quartz gate. The pressure of an inert gas (argon) during the fusion process was ~ 4 atm; fusion temperature (750 ± 10)<sup>0</sup>C. The alloy was held at this temperature for 30 min.

To obtain a thermoelectric base, over stoichiometric tellurium was introduced into the charge in amounts from 0.1 wt. % up to 0.6 wt. % of the weight of the initial charge. The amount of over stoichiometric selenium in the charge varied in the range of 0.05-0.30 wt.%. Experiments have shown that an excess of selenium in the charge has a more effective effect on the thermoelectric properties of the base than the same amount of excess tellurium. [3-5]

Figures 1 and 2 show the effect of an excess of tellurium and selenium, respectively, on changes in the thermoelectric properties of a base synthesized using the technology described above. As can be seen from these data, the optimal amount of superstoichiometric additive, providing the highest values of thermoelectric power  $\alpha^2\sigma$ , for tellurium is 0.18-0.32 wt%, and for selenium is 0.08-0.20 wt%. In this case, the concentration of electrons in the base is  $(0.9^{-1.1}) 10^{19}\text{sm}^{-3}$ .

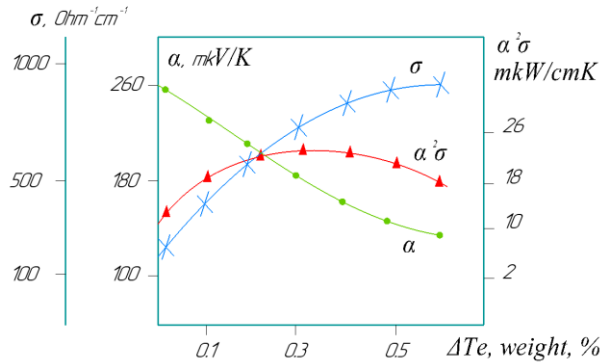


Fig.1. Dependence of thermoelectric properties of the  $\text{Bi}_2\text{Te}_3\text{-Bi}_2\text{Se}_3$  base on the excess of tellurium in the charge

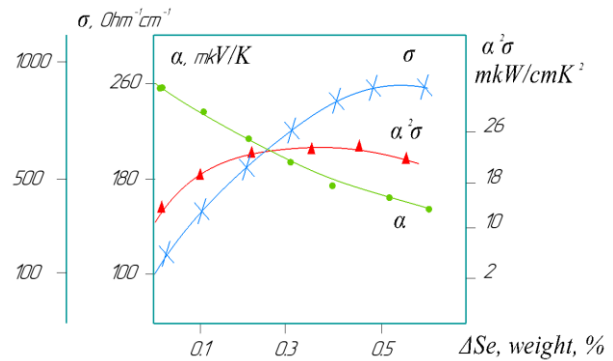


Fig.2. Dependence of the thermoelectric properties of the base in  $\text{Bi}_2\text{Te}_3\text{-Bi}_2\text{Se}_3$  on the selenium excess in the charge.

In order to increase the operating temperature range of the synthesized material  $\text{Bi}_2\text{Te}_3 - \text{Bi}_2\text{Se}_3$ , the developed base was additionally doped. Ammonium iodide salt ( $\text{NH}_4\text{I}$ ) was used as a dopant. As a dopant, ammonium iodide has a number of advantages. Firstly, it is almost not hygroscopic; secondly, it does not decompose when heated up to  $551^\circ\text{C}$ ; thirdly, it does not melt, it sublimates; fourthly, above  $551^\circ\text{C}$ , ammonium iodide decomposes according to the scheme



and the released hydrogen iodide is a much more active chemical reagent than other iodides. In addition, the ammonia released in the reaction plays the role of a reducing agent, reacting with traces of oxides remaining in the charge and eliminating them.

All these advantages of ammonium iodide affect the improvement of the thermoelectric properties of alloys, ensure the reproducibility of the technology during melting.

To determine the effect of the concentration of the introduced dopant on the change in the thermoelectric properties of the base, ammonium iodide was introduced into the charge of the following composition: Bi - 54.1678 wt. %; Te - 39.6923 wt. %; Se -  $(6.1398 + 0.12)$  wt. %. The  $\text{NH}_4\text{I}$  concentration in the charge varied from 0.02 to 0.12 wt. %. Ammonium iodide was loaded into the charge first at the bottom of the crucible. The effect of alloying on the thermoelectric properties of the base is shown in Fig.3.

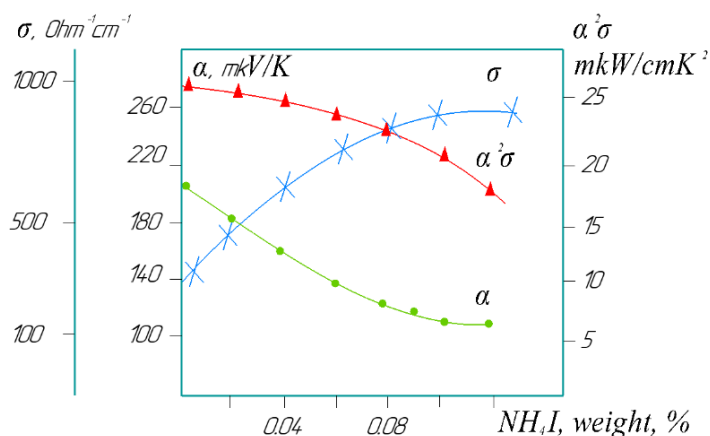


Fig.3. Dependence of thermoelectric properties of the  $\text{Bi}_2\text{Te}_3\text{-Bi}_2\text{Se}_3$  base on the amount of dopant.

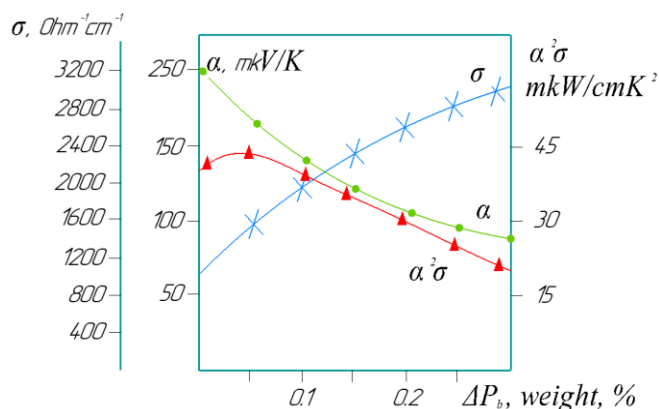


Fig.4. Dependence of thermoelectric properties of the  $\text{Bi}_{2-x}\text{Sb}_x\text{Te}_3$  base on the amount of lead dopant.

According to these data, when the concentration of the alloying addition is changed to 0.08 wt. % thermo - emf coefficient and electrical conductivity have an almost linear relationship. Above this concentration, they almost do not depend on the amount of added  $\text{NH}_4\text{I}$ , which is apparently due to the limited dissolution of iodide ammonium in  $\text{Bi}_2\text{Te}_3 - \text{Bi}_2\text{Se}_3$ .

Optimal thermoelectric properties of alloys for thermogenerator legs are obtained by introducing 0.04 wt. %  $\text{NH}_4\text{I}$ . The parameters of such a base are  $\sigma \approx (950 \pm 30) \text{ Ohm}^{-1}\text{cm}^{-1}$ ,  $\alpha \approx (150 \pm 5) \text{ mV} / \text{K}$ .

#### Obtaining a working substance based on $\text{Bi}_2\text{Te}_3 - \text{Sb}_2\text{Te}_3$

To prepare an alloy of the required composition, the initial components were of the following purity: bismuth GOST 10928 - 64 grade VCh-00, tellurium GOST 9514 - 60 grade TA-1, antimony GOST 1069 - 62 grade C-O and lead C - 00. As a basis for in the study, the composition of the solid solution corresponding to 74%  $\text{Sb}_2\text{Te}_3$  and 26%  $\text{Bi}_2\text{Te}_3$  was selected. The material of the crucible and the shutter was quartz. The charge was loaded as follows. Antimony, tellurium, and bismuth were sequentially loaded at the bottom of the crucible.

To obtain a doped material with hole conductivity in a quartz crucible, the following composition of the charge was taken: Bi - 16.179 wt. %, Te - 56,993 wt. %, Sb - 26.828 wt. %.

As an alloying addition, lead was used in an amount of 0.05 wt. % up to 0.25 wt. %. Thermoelectric properties of materials are shown in Figure 2.4. Optimal thermoelectric properties of the alloy are obtained by introducing an alloying additive of 0.05 - 0.12 wt. %. In this case, the specific electrical

conductivity  $\sigma = (1500-2000) \text{ Ohm}^{-1} \cdot \text{cm}^{-1}$ , the Seebeck coefficient is  $(145-175) \text{ mkV} / \text{K}$ , the concentration of holes is  $(1.5 - 2) \cdot 10^{19} \text{ cm}^{-3}$ .

Table № 1.

$\Delta P_b$ , weight %	Before annealing			After annealing		
	$\sigma, \text{ Ohm}^{-1} \cdot \text{cm}^{-1}$	$\alpha, \text{ mkV/K}$	$\alpha^2 \sigma$ $\text{mkW/cmK}^2$	$\sigma \text{ OM-1}$ $\cdot \text{cm}^{-1}$	$\sigma, \text{ Ohm}^{-1} \cdot \text{cm}^{-1}$	$\alpha, \text{ mkV/K}$
0,10	1800	160	45	1100	195	40
0,20	2250	150	50	1300	190	45
0,25	2600	130	45	1600	160	40
0,30	2800	125	45	1700	160	40
0,40	3000	105	35	2000	135	35

It was found that in the working substance  $\text{Bi}_{2-x}\text{Sb}_x\text{Te}_3\langle\text{Pb}\rangle$ , the parameters are very sensitive to post-technological annealing. To study the effect of annealing, substrates with different lead contents were prepared. The results of measurements of the specific electrical conductivity and thermo-EMF coefficient of the base at  $T = 300 \text{ K}$  before and after annealing are shown in Table 1 (annealing was carried out at temperatures of  $350-400^\circ\text{C}$  for 10 hours).

According to the data in the table, an effective material for thermoelements can be selected using annealing of the fused substance (annealing leads to a decrease in the hole concentration).

Based on the real field of application of the available "AFN-thermo", we will analyze low-temperature materials (up to  $500 \div 550^\circ\text{C}$ ) for thermoelements. These include, first of all,  $\text{Bi}_2\text{Te}_3$  and  $\text{Bi}_2\text{Se}_3$  of stoichiometric composition. Depending on the type of doping,  $\text{Bi}_2\text{Te}_3$  can have either electronic or hole conductivity.  $\text{Bi}_2\text{Te}_3$  is characterized by electronic conductivity. The figure of merit of these materials is respectively equal: (for  $\text{Bi}_2\text{Te}_3$ )  $-Z = 2 \cdot 10^{-3} \text{ deg}^{-1}$  and higher, and (for  $\text{Bi}_2\text{Te}_3$ )  $-Z = 0.8 \cdot 10^{-3} \text{ deg}^{-1}$ .

#### Let's draw brief conclusions:

1. The most effective thermoelectric materials are semiconductors; whose current carriers are close to a degenerate state or even partially degenerate (with a low degree of degeneracy). In this regard, thermoelectric materials should be capable of deep doping (up to carrier concentrations of  $10^{19}-10^{21} \text{ cm}^{-3}$ ).

Theoretical calculation and analysis of the studies carried out in the creation of "AFS-thermo" with volumetric and film thermopiles show that:

To create a thermoelement and a thermopile with the best values of the efficiency, it is necessary to select the optimal ratio of the transverse branches of the TE and the load. In this case,  $\eta_{\text{max}}$  can be achieved in cases of using thermoelectric materials with the best  $Z$ .

Among the existing many materials, the most effective are thermoelectric materials based on the Bi Te Sb - Bi Te Se ternary alloy, obtained by the zone melting method.

It goes without saying that a thermoelectric material must also possess many other physical, mechanical and chemical properties that would ensure the normal operation of the material under conditions of variable temperatures, a given external environment in the presence of mechanical loads. Technological properties, questions of the synthesis of this material and its alloying are also important. One of the essential problems is reliable low-resistance electrical switching of thermoelements. This is one of the most difficult issues of modern practical implementation of the method of direct energy conversion using thermoelectric generators.

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